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In re Application of: JASON P. RHODE and JOHN J. PAULOS

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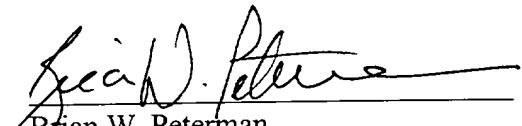
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Respectfully submitted,



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PATENT

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APPLICATION FOR UNITED STATES LETTERS PATENT

for

QUASI-DIFFERENTIAL POWER AMPLIFIER AND METHOD

by

Jason P. Rhode

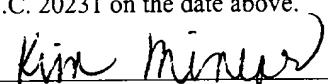
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1

QUASI-DIFFERENTIAL POWER AMPLIFIER AND METHOD

3

4

BACKGROUND OF THE INVENTION

6

1. Field of the Invention

8 The present invention relates to integrated circuit (IC) amplifiers, and more specifically to
9 IC power amplifiers for driving three-wire stereo headphones in small portable stereo systems.

19

2. Description of the Related Art

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Small portable stereo systems generally include a digital audio source, a digital volume control, a digital-to-analog converter (DAC), and an integrated circuit (IC) power amplifier for driving analog output signals to stereo headphones. The vast majority of these stereo headphones have a three-wire connection consisting of a left (L) terminal, a right (R) terminal, a common (C) terminal. The IC power amplifier typically includes a first amplifier that drives a left (L) channel signal connected to the left (L) terminal and a second amplifier that drives a right (R) channel signal connected to the right (R) terminal. The common (C) terminal of the headphone is generally connected to system ground (GND).

2

Because of the low voltage supplies used to power these portable stereo systems, the dynamic range and maximum power delivered by typical power amplifiers to the stereo headphones are limited. For example, with a typical IC power amplifier and a low voltage supply, such as a 3 volt supply, the left (L) and right (R) channel outputs can be driven from approximately 0.5 volts to 2.5 volts. This signal range limits the maximum sine wave that may be delivered to the headphone to about 0.707 volts rms and limits the maximum power into each channel to about $(0.707 \text{ V rms})^2 / 32\Omega = 15 \text{ mW}$. In addition, with a typical IC power amplifier, the left (L) and right (R) terminals must be AC coupled to the IC power amplifier through large capacitors to provide a low frequency pole for the left (L) and right (R) headphone speakers. For

1 example, assuming right (R) and left (L) headphone speakers having a typical value of about
2 32Ω , the coupling capacitors must be about $100 \mu\text{F}$ to place the low frequency RC pole at about
3 50 Hz. The cost of two large capacitors, such as $100 \mu\text{F}$ capacitors, is a significant problem for
4 these types of systems.

5
6 To eliminate the need for the AC coupling capacitors, a third amplifier may be added to
7 the IC power amplifier to drive the common (C) terminal of the headphone at a fixed common
8 mode (CM) voltage (V_{CM}). This fixed common mode driver approach, however, requires that the
9 third amplifier have approximately twice the current drive capability of the left (L) channel and
10 right (R) channel amplifiers at peak current loads. This additional high power third amplifier
11 significantly increases the power consumption of the IC power amplifier and does not increase
12 the maximum power deliverable to the headphone. For example, in a typical system, there is a
13 particular volume control setting that will cause the power amplifier to just barely clip the signal
14 when given a full scale signal from the digital audio source. Because the program material being
15 processed by the digital audio source typically does not contain any full scale signals, the volume
16 control will often have settings that exceed this clipping limit. Assuming that the output of the
17 right (R) and left (L) channel drive amplifiers can swing from $V_{CM} - 1$ volts to $V_{CM} + 1$ volts
18 without clipping, the maximum voltage that the IC power amplifier in the fixed common mode
19 approach can deliver to the headphones without clipping is about $2 V_{pp}$ (volts peak-to-peak).

20
21 **SUMMARY OF THE INVENTION**

22
23 In accordance with the present invention, a quasi-differential power amplifier enhances
24 drive capability and dynamic range by providing a first output signal, a second output signal, and
25 a common mode output signal that are each a combination of a first and a second input signals.
26 In one embodiment, the common mode output signal is used as feedback to the first and second
27 output signals. In a further embodiment, the input signals are digital, and the quasi-differential
28 power amplifier includes a first and second digital-to-analog converters coupled to the first and
29 second input signals, a first amplifier driving the first output signal, a second amplifier driving
30 the second output signal, and a third amplifier driving the common mode output signal. In one

1 application, the input signals are a right and left channel audio input signals, and the output
2 signals are used to drive three-wire stereo headphones.

3

4 **BRIEF DESCRIPTION OF THE DRAWINGS**

5

6 FIG. 1 is a block diagram of a system including a quasi-differential power amplifier
7 according to the present invention.

8

9 FIG. 2 is a block diagram of an embodiment for a quasi-differential power amplifier
10 according to the present invention.

11

12 FIG. 3 is a block diagram of an alternative embodiment for a quasi-differential power
13 amplifier according to the present invention.

14

15 FIG. 4 is a circuit configuration for the quasi-differential power amplifier depicted in
16 FIG. 3.

17

18 FIG. 5 is a block diagram of another alternative embodiment of a quasi-differential power
19 amplifier according to the present invention.

20

21 **DESCRIPTION OF THE PREFERRED EMBODIMENTS**

22

23 Referring to FIG. 1, a system 150 is shown that includes a quasi-differential power
24 amplifier 100 connected to a digital-to-analog converter (DAC) 106 and three-wire headphones
25 108. System 150 also includes a digital audio source 102 connected to a digital volume control
26 block 104, which is in turn connected to a DAC 106. The digital audio source 102 provides a left
27 (L) channel output 124 and a right (R) channel output 126 to the digital volume control 104,
28 which in turn provides a volume adjusted left (L) channel output 120 and a volume adjusted right
29 (R) channel output 122 to the DAC 106. The DAC 106 provides an analog left (L) channel
30 output 116 and an analog right (R) channel output 118 to the quasi-differential power amplifier

1 100. The quasi-differential power amplifier 100 drives the three input terminals of the
2 headphone 108 with left (L) channel signal 112, right (R) channel signal 110, and common mode
3 (CM) signal 114.

4

5 In one embodiment, the system 150 may be a small portable stereo system including
6 three-wire stereo headphones 108. It is noted that the embodiment for system 150 depicted in
7 FIG. 1 is an example embodiment and that alternative implementations could be designed and
8 utilized. For example, the left (L) channel output 116 and right (R) channel output 118 could be
9 any two signals desired to be input to the quasi-differential power amplifier 100, and the left (L)
10 channel signal 112, right (R) channel signal 110, and common mode (CM) signal 114 could be
11 the output signals of the quasi-differential power amplifier 100. Thus, the input and output
12 signals are not required to relate to a left (L) and right (R) channel stereo signal.

13

14 FIG. 2 shows an embodiment for a quasi-differential power amplifier 100 according to
15 the present invention. The analog left (L) channel output 116 from DAC 106 is connected as a
16 positive input to adders 210 and 216 and is connected as a negative input to adder 214. The
17 analog right (R) channel output 118 from DAC 106 is connected as a positive input to adders 214
18 and 218 and is connected as a negative input to adder 210. A common mode voltage (V_{CM}) 226
19 is connected as a negative input to adders 216 and 218. The outputs of adders 216 and 218 are
20 connected as positive inputs to adder 212. The outputs 232, 234, and 236 of adders 210, 212,
21 and 214 are connected to amplifiers 202, 204, and 206, respectively, which each have an inverted
22 gain of $-1/2$. The outputs of amplifiers 202, 204, and 206 are connected as positive inputs to
23 adders 220, 224, and 222, respectively, which also receive the common mode voltage (V_{CM}) 226
24 as a positive input. The output of adder 220 is the right (R) channel signal 110; the output of
25 adder 222 is the left (L) channel signal 112; and the output of adder 224 is the common mode
26 (CM) signal 114. To simplify FIG. 2, the left (L) and right (R) channel analog audio inputs 116
27 and 118 from DAC 106 are shown as single-ended signals, although it is understood that these
28 signals may be implemented as differential or single-ended signals, as desired.

29

1 In operation, the left (L) channel analog audio input 116 from DAC 106 consists of a
 2 signal voltage (V_L) plus a common mode voltage (V_{CM}). Similarly, the right (R) channel analog
 3 audio input 118 from DAC 106 consists of a signal voltage (V_R) plus a common mode voltage
 4 (V_{CM}). Although analog audio inputs 116 and 118 are shown as single lines in FIG. 2, it is
 5 understood that they may be implemented as differential signals, allowing them to swing 4 V_{pp} .
 6 The output 232 of adder 210 is $(V_L + V_{CM}) - (V_R + V_{CM}) = V_L - V_R$. The output 236 of adder
 7 214 is $(V_R + V_{CM}) - (V_L + V_{CM}) = V_R - V_L$. The output 234 of adder 212 is $(V_R + V_{CM}) + (V_L +$
 8 $V_{CM}) - 2V_{CM} = V_R + V_L$. The left (L) channel output signal (L_{OUT}) 112 from adder 222, the right
 9 (R) channel output signal (R_{OUT}) 110 from adder 220, and the common mode (CM) output signal
 10 (CM_{OUT}) 114 from adder 226 are as follows:

11 $L_{OUT} = V_{CM} + (V_L - V_R)/2$;

12 $R_{OUT} = V_{CM} + (V_R - V_L)/2$; and

13 $CM_{OUT} = V_{CM} - (V_L + V_R)/2$.

14 The signals which are actually applied to the right and left speakers of the headphone 108 are the
 15 following:

16 $L_{speaker} = L_{OUT} - CM_{OUT} = [V_{CM} + (V_L - V_R)/2] - [V_{CM} - (V_L + V_R)/2] = V_L$; and

17 $R_{speaker} = R_{OUT} - CM_{OUT} = [V_{CM} + (V_R - V_L)/2] - [V_{CM} - (V_R + V_L)/2] = V_R$.

18
 19 Although it is not practical to drive the left (L) and right (R) terminals of the headphone
 20 fully differentially, the quasi-differential power amplifier of the present invention provides
 21 substantially greater drive capability and increased dynamic range and reduces power
 22 consumption compared to prior single-ended drive techniques, such as those used by prior
 23 grounded power amplifier and fixed common mode amplifier approaches. The quasi-differential
 24 power amplifier of the present invention achieves these advantages by providing a left channel
 25 output signal, a right channel output signal, and a common mode output signal that are each a
 26 combination of the left and right channel input signals.

27
 28 An example of this advantage may be seen in the situation where $V_L = V_{CM} + 2$ volts and
 29 $V_R = V_{CM}$. Assuming these values, CM_{OUT} and R_{OUT} will both be driven to values of $V_{CM} - 1$ volt,
 30 while L_{OUT} will be driven to a value of $V_{CM} + 1$ volt. As desired, a 2 volt signal will ultimately be

1 applied to the left speaker, while a 0 volt signal is applied to the right speaker. Thus, for the
2 quasi-differential power amplifier of the present invention, a non-clipped signal will be applied
3 to each speaker. In contrast, for the prior grounded power amplifier and fixed common mode
4 amplifier approaches, a clipped signal of +1 volt would be applied to the left speaker due to
5 clipping of the V_L signal to $V_{CM} + 1$ volt, and a 0 volt signal would be applied to the right
6 speaker. This case illustrates, therefore, the potential for increased signal swing available
7 utilizing the quasi-differential power amplifier according to the present invention.

8

9 One potential drawback for the embodiment depicted in FIG. 2, however, is that the
10 signal level which causes the right (R) channel to clip is dependent on the signal level in the left
11 (L) channel and vice versa. Assuming that the output of the right channel signal (R_{OUT}) 110 and
12 left channel signal (L_{OUT}) 112 can swing from $V_{CM} - 1$ volts to $V_{CM} + 1$ volts without clipping,
13 the power amplifier 100 will clip whenever the instantaneous value of $|V_L - V_R| > 2$. Three
14 different signal level conditions illustrate example clipping situations. In a first case, assuming
15 $|V_L|$ and $|V_R| \leq 1$ volt, neither output channel will be clipped, regardless of polarity of the
16 signals. In a second case, assuming $V_L = +2$ volts and $V_R = -2$ volts, CM_{OUT} will be driven to a
17 value of V_{CM} . Ideally without clipping, L_{OUT} and R_{OUT} would be driven to $V_{CM} + 2$ volts and V_{CM}
18 - 2 volts, respectively. Because L_{OUT} will clip at $V_{CM} + 1$ volt and R_{OUT} will clip at $V_{CM} - 1$ volt,
19 however, a clipped signal will ultimately be applied to each speaker. An analogous situation
20 occurs if $V_L = -2$ volts and $V_R = +2$ volts. In a third case, assuming V_L and $V_R = +2$ volts,
21 CM_{OUT} would be ideally driven to a value of $V_{CM} - 2$ volts, but will clip at $V_{CM} - 1$ volt. Because
22 the L_{OUT} and R_{OUT} signals will both be at V_{CM} , a clipped signal will ultimately be delivered to
23 both speakers. An analogous situation occurs when both V_L and $V_R = -2$ volts.

24

25 Considering the above clipping situations, the embodiment of FIG. 2 will encounter
26 clipping for two primary reasons — large signals of opposite polarity (case two) and large
27 signals of the same polarity (case three). In second case situations, the clipping occurs at the
28 L_{OUT} and R_{OUT} terminals. In third case situations, the clipping occurs at the CM_{OUT} terminal,
29 while the L_{OUT} and R_{OUT} terminals are at V_{CM} . By incorporating a mechanism to detect clipping
30 on the CM_{OUT} terminal and to adjust the L_{OUT} and R_{OUT} terminals to compensate, the third case

1 clipping situation may be avoided. As discussed further below, second case situations are
2 relatively rare and are less of a concern.

3

4 FIG. 3 shows an alternative embodiment for a quasi-differential headphone power
5 amplifier 100 that provides a feedback mechanism to compensate for third case clipping
6 situations. The analog left (L) channel output 116 from DAC 106 is connected as a positive
7 input to adder 301, and the analog right (R) channel output 118 from DAC 106 is connected as a
8 positive input to adder 303. Adders 303 and 301 also receive the common mode voltage (V_{CM})
9 226 as a negative input. The output 312 of adder 303 is connected as a positive input to adders
10 210 and 212. The output 314 of adder 303 is connected as a positive input to adders 214 and
11 212. The output 320 of adder 212 is connected to amplifier 204, which has a negative gain of $-\frac{1}{2}$. The output of amplifier 204 is connected as a positive input to adders 210 and 214. The
12 outputs 316 and 318 of adders 210 and 214 are connected to amplifiers 202 and 206,
13 respectively, which each have a positive gain of +1. The outputs of amplifiers 202, 204, and 206
14 are connected as positive inputs to adders 220, 224, and 222, respectively, which also receive the
15 common mode voltage (V_{CM}) 226 as a positive input. As in FIG. 2, the output of adder 220 is the
16 right (R) channel signal 110; the output of adder 222 is the left (L) channel signal 112; and the
17 output of adder 224 is the common mode (CM) signal 114.

19

20 In operation, a portion of the CM_{OUT} signal from the output of amplifier 204 is provided
21 as feedback to adders 210 and 214. This feedback is combined with the left (L) and right (R)
22 channel signals to adjust the resulting L_{OUT} and R_{OUT} signal levels to compensate for any clipping
23 which may occur at the CM_{OUT} terminal. As with FIG. 2, the left (L) channel analog audio input
24 116 from DAC 106 consists of a signal voltage (V_L) plus a common mode voltage (V_{CM}). Similarly,
25 the right (R) channel analog audio input 118 from DAC 106 consists of a signal voltage (V_R) plus a common mode voltage (V_{CM}). The output 314 of adder 301 is $(V_L + V_{CM}) - V_{CM} = V_L$. The output 312 of adder 303 is $(V_R + V_{CM}) - V_{CM} = V_R$. The output 320 of adder 212
26 is $V_L + V_R$ and is applied to amplifier 204. Amplifier 204 produces an output signal 322 that is
27 used as a feedback (FB) signal to the left and right signal paths. The output 322 is $FB = (-\frac{1}{2})(V_L$
28
29

1 $+ V_R$). The amplifier 204, and therefore the output signal 322, may be assumed to clip at certain
 2 values such as +1 volt or -1 volt.

3

4 The output 318 of adder 214 is $V_L + FB$. In a non-clipped situation, $FB = (-\frac{1}{2})(V_L + V_R)$,
 5 and the output 318 will be $V_L + FB = V_L + (-\frac{1}{2})(V_L + V_R) = (V_L - V_R)/2$. Similarly, the output
 6 316 of adder 210 is $V_R + FB$. In a non-clipped situation, $FB = (-\frac{1}{2})(V_L + V_R)$, and the output 316
 7 will be $V_R + FB = V_R + (-\frac{1}{2})(V_L + V_R) = (V_R - V_L)/2$. The output 318 is fed to amplifier 206 to
 8 provide output 324, and output 316 is fed to amplifier 202 to provide output 326. As with
 9 amplifier 204 above, amplifiers 202 and 206 may be assumed to clip at certain values such as +1
 10 volt or -1 volt.

11

12 In non-clipped situations, the left (L) channel output signal (L_{OUT}) 112 from adder 220,
 13 the right (R) channel output signal (R_{OUT}) 110 from adder 224, and the common mode (CM)
 14 output signal (CM_{OUT}) 114 from adder 226 are as follows:

15 $L_{OUT} = V_{CM} + (V_L - V_R)/2$;

16 $R_{OUT} = V_{CM} + (V_R - V_L)/2$; and

17 $CM_{OUT} = V_{CM} - (V_L + V_R)/2$.

18 The signals which are actually applied to the right and left speakers of the headphone 108 in non-
 19 clipped situations are the following:

20 $L_{speaker} = L_{OUT} - CM_{OUT} = [V_{CM} + (V_L - V_R)/2] - [V_{CM} - (V_L + V_R)/2] = V_L$; and

21 $R_{speaker} = R_{OUT} - CM_{OUT} = [V_{CM} + (V_R - V_L)/2] - [V_{CM} - (V_R + V_L)/2] = V_R$.

22

23 For the embodiment of FIG. 3 and again assuming clipping at $V_{CM} \pm 1$ volt, the signal
 24 applied across the left and right speakers will clip whenever the instantaneous value of $|V_L - V_R|$
 25 > 2 , or when $|V_L|$ or $|V_R| > 2$. Considering the third case situation above for this
 26 embodiment with V_L and $V_R = + 2$ volts, the CM_{OUT} signal would ideally be driven to $V_{CM} - 2$
 27 volts, and the L_{OUT} signal and the R_{OUT} signal would ideally be driven to V_{CM} . According to the
 28 equations above, therefore, the desired resulting ideal signals to the left and right speakers are
 29 $L_{speaker} = R_{speaker} = +2$ volts. Because of clipping in the amplifier 204, however, the output signal

1 322 of amplifier 204 will be clipped to -1 volt, and the CM_{OUT} signal will be clipped to $V_{CM} - 1$
2 volt.

3

4 The feedback (FB) signal 322 applied to adders 210 and 214 in the left and right channel
5 paths compensates for this clipping condition. Because this feedback signal is also not ideal,
6 having been clipped at -1 volt, the output 316 of adder 210 and the output 318 of adder 214 will
7 adjust to +1 volt instead of an ideal 0 volts. For this clipped situation, therefore, the left and right
8 channel output signals 112 (L_{OUT}) and 110 (R_{OUT}) will adjust to produce $L_{OUT} = R_{OUT} = V_{CM} + 1$
9 volt instead of the ideal V_{CM} volts. The resulting signal actually sent to the left and right
10 speakers will then be $L_{speaker} = L_{OUT} - CM_{OUT} = (V_{CM} + 1) - (V_{CM} - 1) = +2$ volts, and $R_{speaker} =$
11 $R_{OUT} - CM_{OUT} = (V_{CM} + 1) - (V_{CM} - 1) = +2$ volts. Thus, the present invention provides the
12 desired resulting signal to the left and right speakers even though the common mode output
13 signal was clipped at $V_{CM} - 1$ volt.

14

15 The quasi-differential power amplifier of the present invention, therefore, provides
16 particularly advantageous results for case three situations where audio program material contains
17 a large imbalance in signal levels or that contains signals in which the peak excursions are
18 largely in phase with each other. For case two situations, in which signals have peak excursions
19 which are perfectly out of phase, the quasi-differential power amplifier of the present invention
20 does not tend to improve performance and clips at substantially the same point as the fixed
21 common mode voltage approach. However, actual peak levels in the material being processed by
22 the digital audio source occur infrequently and are perfectly out of phase with each other only a
23 small percentage of the time. Thus, case two situations are less of a concern.

24

25 Referring now to FIG. 4, a circuit implementation is shown for the quasi-differential
26 headphone power amplifier 100 depicted in the block diagram of FIG. 3. DAC 106 includes a
27 left (L) channel path DAC 402 and a right (R) channel path DAC 404 that drive the power
28 amplifier 100. DACs 402 and 404 may be fully-differential switched-capacitor DACs. The
29 volume adjusted left (L) channel output 120 is an input to the left (L) channel DAC 402.
30 Similarly, the volume adjusted right (R) channel output 122 is an input to the right (R) channel

1 DAC 404. Common mode voltage (V_{CM}) 226 is an additional input to both left (L) channel DAC
2 402 and right (R) channel DAC 404. The positive and negative outputs of left (L) channel DAC
3 402 make up the analog left (L) channel output 116 from DAC 106, which is a differential input
4 to quasi-differential power amplifier 100. The positive and negative outputs of right (R) channel
5 DAC 404 make up the analog right (R) channel output 118 from DAC 106, which is a
6 differential input to the quasi-differential power amplifier 100. It is noted that the embodiment
7 for DAC 106 depicted in FIG. 4 is an example embodiment and that alternative implementations
8 including a larger or smaller number of DACs or different DAC circuitry could be designed and
9 utilized.

10

11 Quasi-differential power amplifier 100 includes a left (L) channel operational amplifier
12 (OPAMP) 410 driving the left (L) channel signal 112, a right (R) channel OPAMP 414 driving
13 the right (R) channel signal 110, and a common mode OPAMP 412 driving the common mode
14 (CM) signal 114. OPAMPs 410, 412, and 414 are connected to a power supply (V_{dd}) 420, which
15 may be 3 volts, and a circuit ground (GND) 422. The negative differential output of left (L)
16 channel DAC 402 is connected to the negative input terminal of OPAMP 410 through a resistor
17 432. The positive differential output of left (L) channel DAC 402 is connected through a resistor
18 434 to the positive input terminal of OPAMP 410 and through a resistor 438 to a negative input
19 terminal of OPAMP 412. The negative differential output of right (R) channel DAC 404 is
20 connected to the negative input terminal of OPAMP 414 through a resistor 446. The positive
21 differential output of right (R) channel DAC 404 is connected through a resistor 444 to the
22 positive input terminal of OPAMP 414 and through a resistor 440 to a negative input terminal of
23 OPAMP 412. As feedback, the output of OPAMP 412 is connected to the negative input
24 terminal of OPAMP 412 through resistor 442, to the positive input terminal of OPAMP 410
25 through resistor 448, and to the positive input of OPAMP 414 through resistor 450. The resistors
26 432, 434, 436, 438, 440, 442, 444, 446, 448, and 450 may be matched resistors. It is noted that
27 the embodiment for quasi-differential power amplifier 100 depicted in FIG. 4 is an example
28 embodiment and that alternative implementations including a larger or smaller number of
29 amplifiers or different amplifier circuitry could be designed and utilized.

30

1 The three-wire headphones 108 include a left (L) channel speaker represented by resistor
 2 (R_{LEFT}) 406 and a right (R) channel speaker represented by resistor (R_{RIGHT}) 408, which may each
 3 be 32Ω . Resistor (R_{LEFT}) 406 is connected between the left (L) channel signal 112, which is
 4 driven by the left (L) channel OPAMP 414, and to the common mode (CM) signal 114, which is
 5 driven by the common mode OPAMP 412. Resistor (R_{RIGHT}) 408 is connected between the right
 6 (R) channel signal 110, which is driven by the right (R) channel OPAMP 414, and the common
 7 mode (CM) signal 114, which is driven by the common mode OPAMP 412.

8

9 In operation, the left (L) channel path DAC 402 provides a positive differential output
 10 (V_{L+}) and a negative differential output (V_{L-}), and the right (R) channel path DAC 404 provides a
 11 positive differential output (V_{R+}) and a negative differential output (V_{R-}). The common mode
 12 signal output (CM_{OUT}) 114 driven by OPAMP 412 is $CM_{OUT} = V_{CM} - V_{R+} - V_{L+}$. This signal is
 13 fed back to OPAMP 410 and OPAMP 414 and is used as a reference signal for the differential to
 14 single-ended conversion performed by OPAMP 410 and OPAMP 414. The output signal (L_{OUT})
 15 of the left channel OPAMP 410 is $L_{OUT} = V_{L+} - V_{L-} + CM_{OUT}$. In ideal situations without clipping
 16 of CM_{OUT} , L_{OUT} will be $L_{OUT} = V_{CM} - V_{R+} - V_{L-}$. Similarly, the output signal (R_{OUT}) of the right
 17 channel OPAMP 414 is $R_{OUT} = V_{R+} - V_{R-} + CM_{OUT}$. And in ideal situations without clipping,
 18 R_{OUT} will be $R_{OUT} = V_{CM} - V_{L+} - V_{R-}$. In a non-clipping situation, therefore, the signals which are
 19 actually applied to the right and left speakers 406 and 408 of the headphone 108 are the
 20 following:

$$21 \quad L_{speaker} = L_{OUT} - CM_{OUT} = [V_{CM} - V_{R+} - V_{L-}] - [V_{CM} - V_{R+} - V_{L+}] = V_{L+} - V_{L-}; \text{ and}$$

$$22 \quad R_{speaker} = R_{OUT} - CM_{OUT} = [V_{CM} - V_{L+} - V_{R-}] - [V_{CM} - V_{R+} - V_{L+}] = V_{R+} - V_{R-}.$$

23 These outputs correlate to the differential output of the DACs 402 and 404, which could
 24 potentially swing $4 V_{pp}$.

25

26 Similar to the discussion above with respect to FIG. 3, the embodiment of the present
 27 invention depicted in FIG. 4 handles certain clipping conditions on CM_{OUT} through the use of the
 28 CM_{OUT} signal as feedback to the right and left channel signals. For example, assuming the $V_{R+} =$
 29 $V_{L-} = +1$ volts and the $V_{R-} = V_{L+} = -1$ volts, CM_{OUT} would ideally be driven to $CM_{OUT} = V_{CM} - 2$
 30 volts, and L_{OUT} and R_{OUT} would ideally be driven to $L_{OUT} = R_{OUT} = V_{CM}$. Thus, without clipping,

1 the signals actually applied to the left and right speakers would be $R_{\text{speaker}} = L_{\text{speaker}} = +2$ volts.
2 Assuming now that CM_{OUT} clips at $V_{\text{CM}} - 1$ volts, L_{OUT} and R_{OUT} will adjust accordingly so that
3 the resulting speaker output signals are still ideal. In particular, L_{OUT} will adjust such that $L_{\text{OUT}} =$
4 $V_{L-} - V_{L+} + CM_{\text{OUT}} = +1 - (-1) + (V_{\text{CM}} - 1) = V_{\text{CM}} + 1$ volts. Similarly, R_{OUT} will adjust such that
5 $R_{\text{OUT}} = V_{R-} - V_{R+} + CM_{\text{OUT}} = +1 - (-1) + (V_{\text{CM}} - 1) = V_{\text{CM}} + 1$ volts. Even with clipping as
6 assumed above, therefore, the signals actually applied to the left and right speakers according to
7 the embodiment of the present invention in FIG. 4 will be $R_{\text{speaker}} = L_{\text{speaker}} = +2$ volts.

8

9 It should be noted that rather than an analog implementation, the quasi-differential
10 approach of the present invention could be implemented in the digital data path. In this case,
11 DACs and amplifiers could be used to drive the outputs of digital processors to the desired signal
12 output levels. This digital approach has the advantage that the differential to single-ended signal
13 combination is performed in the digital domain, but has the disadvantage of requiring additional
14 DACs.

15

16 FIG. 5 depicts an example embodiment 500 for such a digital path approach for a quasi-
17 differential power amplifier according to the present invention. Signal 502 may be a digital left
18 (L) channel audio input signal, and signal 504 may be a digital right (R) channel audio input
19 signal. A common mode digital processor 504 may receive both the digital left (L) and right (R)
20 channel audio input signals 502 and 504. The common mode digital processor 504 may process
21 these two input signals as desired and provide an output signal 512 that is dependent upon the
22 left (L) and right (R) channel audio input signals 502 and 504. This common mode output signal
23 512 may then be used as the feedback signal to the left and right channel signal paths.

24

25 The left channel digital processor 506 may receive the digital left (L) channel audio input
26 signal 502 and the feedback signal 512. The left channel digital processor 506 may process these
27 two input signals as desired and provide an output signal 507 that is dependent upon the left (L)
28 channel input signal 502 and the common mode feedback signal 512. Similarly, the right
29 channel digital processor 510 may receive the digital right (R) channel audio input signal 504
30 and the feedback signal 512. The right channel digital processor 510 may process these two

1 input signals as desired and provide an output signal 511 that is dependent upon the right (R)
2 channel input signal 504 and the common mode feedback signal 512. Because the common
3 mode feedback signal 512 is dependent upon both the left (L) and right (R) channel audio input
4 signals 502 and 504, the output signal 507 from the left channel digital processor 506 and the
5 output signal 511 from the right channel digital processor 510 are also dependent upon both the
6 left (L) and right (R) channel audio input signals 502 and 504.

7

8 DACs 514, 516 and 518 may be used to convert the digital processor output signals 507,
9 512 and 511, respectively, to analog signals. Amplifiers 520, 522 and 524 may be connected to
10 DACs 514, 516 and 518, respectively, to drive the left channel output signal 526, the common
11 mode output signal 528, and the right channel output signal 530.

12

1 **WHAT IS CLAIMED IS:**

2

3 1. An audio system having reduced clipping effects, comprising:
4 an audio source producing left and right channel input signals; and
5 drive circuitry coupled to said left and right channel input signals and producing a left
6 channel output signal, a right channel output signal, and a common mode output
7 signal that are each dependent upon a combination of said left and said right
8 channel input signals so that clipping effects are reduced.

9

10 2. The audio system of claim 1, wherein said left channel output signal and said right
11 channel output signal are dependent upon feedback from said common mode output signal.

12

13 3. The audio system of claim 2, further comprising three-wire stereo headphones coupled to
14 said drive circuitry.

15

16 4. The audio system of claim 3, wherein said audio system is a portable audio system.

17

18 5. The audio system of claim 2, wherein said left and right channel input signals from said
19 audio source are digital signals.

20

21 6. The audio system of claim 5, wherein said drive circuitry comprises a first amplifier
22 driving said left channel output signal, a second amplifier driving said right channel output
23 signal, and a third amplifier driving said common mode output signal.

24

25 7. The audio system of claim 6, wherein said drive circuitry further comprises a first and a
26 second digital-to-analog converters coupled to said digital left and right channel input signals,
27 and wherein said first, second and third amplifiers receive analog left and right channel input
28 signals from said first and second digital-to-analog converters.

29

1 8. The audio system of claim 5, wherein said drive circuitry comprises a left channel digital
2 processor providing said left channel output signal, a right channel digital processor providing
3 said right channel output signal, and a common mode digital processor providing said common
4 mode output signal.

5

6 9. The audio system of claim 8, further comprising:
7 a first digital-to-analog converter and a first amplifier coupled to said left channel digital
8 processor to drive said left channel output signal;
9 a second digital-to-analog converter and a second amplifier coupled to said right channel
10 digital processor to drive said right channel output signal; and
11 a third digital-to-analog converter and a third amplifier coupled to said common mode
12 digital processor to drive said common mode output signal.

13
14
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20

14 10. A quasi-differential amplifier having reduced clipping effects, comprising:
15 a first and a second analog input signals; and
16 a plurality of amplifiers receiving said first and said second analog input signals and
17 producing a first output signal, a second output signal, and a common mode
18 output signal that are each dependent upon a combination of said first and said
19 second analog input signals so that clipping effects are reduced.

21 11. The quasi-differential amplifier of claim 10, wherein said first and second output signals
22 are dependent upon feedback from said common mode output signal.

23
24 12. The quasi-differential amplifier of claim 11, wherein said plurality of amplifiers include a
25 first amplifier to drive said first output signal, a second amplifier to drive said second output
26 signal, and a third amplifier to drive said common mode output signal.

27
28 13. The quasi-differential amplifier of claim 12, wherein an output of said third amplifier is
29 coupled as an input to said first and said second amplifiers.

30

1 14. The quasi-differential amplifier of claim 11, wherein said first and second analog input
2 signals are differential signals and said plurality of amplifiers provide single-ended output
3 signals.

4

5 15. The quasi-differential amplifier of claim 11, wherein said first and second analog input
6 signals comprise left and right channel audio input signals and said first and second output
7 signals are left and right channel audio output signals.

8

9 16. The quasi-differential amplifier of claim 15, wherein said left channel output signal, said
10 right channel output signal, and said common mode output signal are capable of driving three-
11 wire stereo headphones.

12

13 17. A drive circuit receiving a first and a second input signals and driving a first output
14 signal, a second output signal, and a common mode output signal that are each dependent upon a
15 combination of said first and second input signals so that clipping effects are reduced.

16

17 18. The drive circuit of claim 17, wherein said first and second output signals are dependent
18 upon feedback from said common mode output signal.

19

20 19. The drive circuit of claim 18, comprising a first amplifier to drive said first output signal,
21 a second amplifier to drive said second output signal, and a third amplifier to drive said common
22 mode output signal

23

24 20. The drive circuit of claim 19, wherein said first and second input signals comprise right
25 and left channel audio input signals.

26

27 21. The drive circuit of claim 20, wherein said left and right channel input signals comprise
28 digital signals.

29

1 22. The drive circuit of claim 21, further comprising a first digital-to-analog converter
2 coupled to said left channel input signal and a second digital-to-analog converter coupled to said
3 right channel input signal, and wherein said first, second and third amplifiers receive analog left
4 and right channel input signals from said first and second digital-to-analog converters.

5

6 23. The drive circuit of claim 21, further comprising a left channel digital processor
7 providing said left channel output signal, a right channel digital processor providing said right
8 channel output signal, and a common mode digital processor providing said common mode
9 output signal.

10

11 24. The drive circuit of claim 23, further comprising:
12 a first digital-to-analog converter and said first amplifier coupled to said left channel
13 digital processor to drive said left channel output signal;
14 a second digital-to-analog converter and said second amplifier coupled to said right
15 channel digital processor to drive said right channel output signal; and
16 a third digital-to-analog converter and third amplifier coupled to said common mode
17 digital processor to drive said common mode output signal.

18

19 25. A method for driving multiple outputs with a quasi-differential signal to reduce clipping
20 effects, comprising:
21 receiving a first and a second input signals; and
22 producing a first output signal, a second output signals, and a common mode output
23 signal that are each dependent upon a combination of said first and second input
24 signals so that clipping effects are reduced.

25

26 26. The method of claim 25, further comprising providing said common mode output signal
27 as feedback to said first and second output signals such that said first and second output signals
28 are dependent upon feedback from said common mode output signal.

29

1 27. The method of claim 25, wherein said first and second input signals comprise a left and
2 right channel audio input signals.

3

4 28. The method of claim 27, wherein said audio input signals are digital signals and further
5 comprising converting said digital audio input signals into analog audio input signals prior to
6 said producing step.

7

8 29. The method of claim 27, wherein said first output signal, said second output signal and
9 said common mode signals are digital signals and further comprising converting said digital
10 output signals into analog output signals after said producing steps.

11

12 30. The method of claim 27, further comprising utilizing said left channel output signal, said
13 right channel output signal, and said common mode output signal to drive three-wire stereo
14 headphones

15

1

2 **QUASI-DIFFERENTIAL POWER AMPLIFIER AND METHOD**

3

4

5 **ABSTRACT OF THE DISCLOSURE**

6

7 A quasi-differential power amplifier and method are disclosed that enhance drive
8 capability and dynamic range by driving a right, left and common terminals with a right channel
9 output signal, a left channel output signal, and a common mode output signal that are each a
10 combination of the left and right channel input signals. In addition, the common mode output
11 signal may be used as feedback so that the left and right channel output signals so that these
12 signals are dependent upon feedback from the common mode output signal. The quasi-
13 differential power amplifier may include a first amplifier driving the left channel output signal, a
14 second amplifier driving the right channel output signal, and a third amplifier driving the
15 common mode output signal. In one application, the quasi-differential amplifier may be used to
16 drive three-wire stereo headphones for use in small portable stereo systems.

17

18

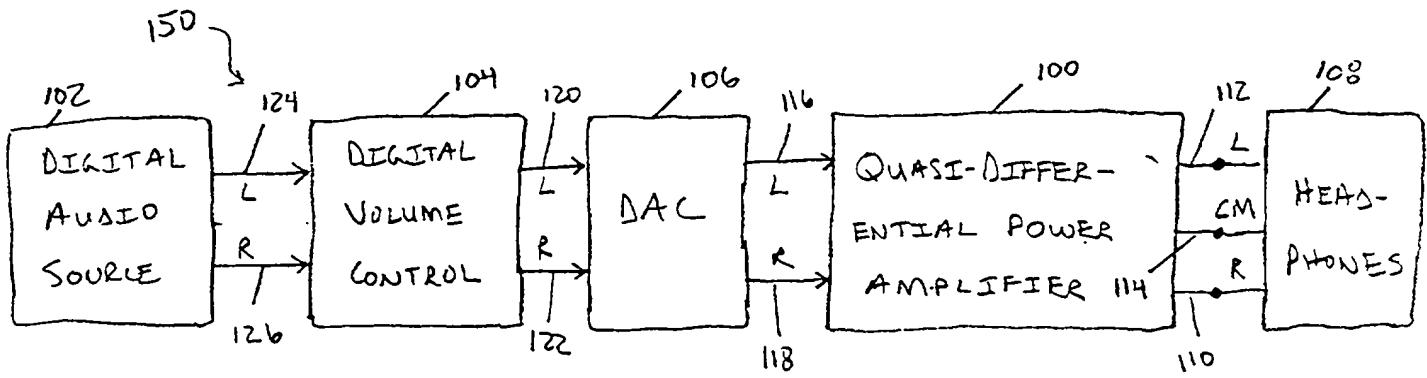


FIG. 1

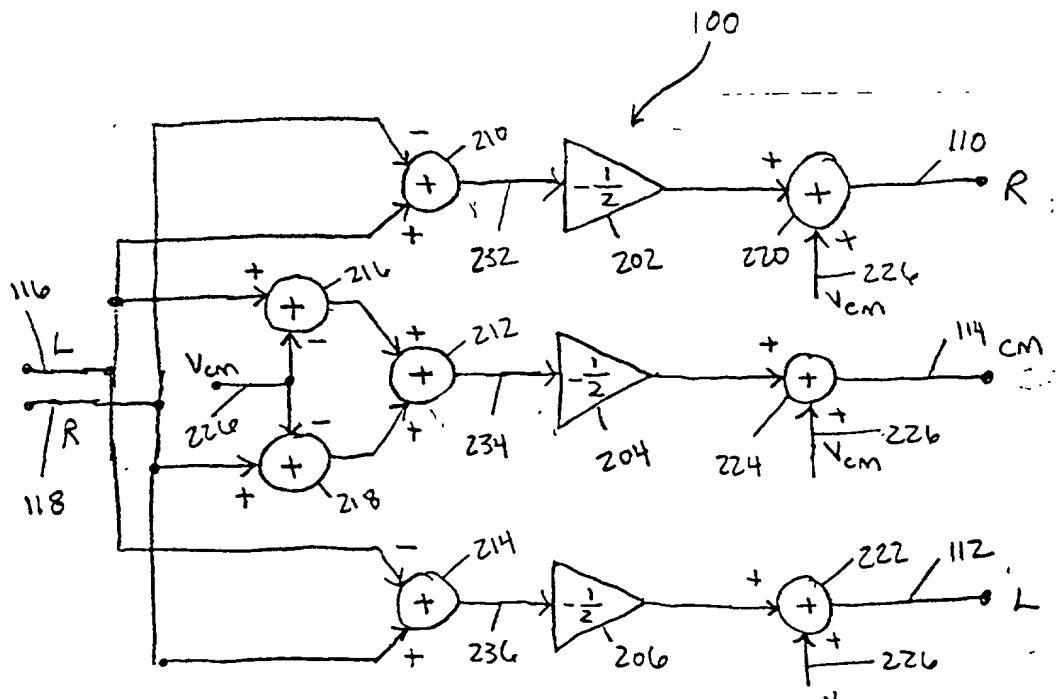


FIG. 2

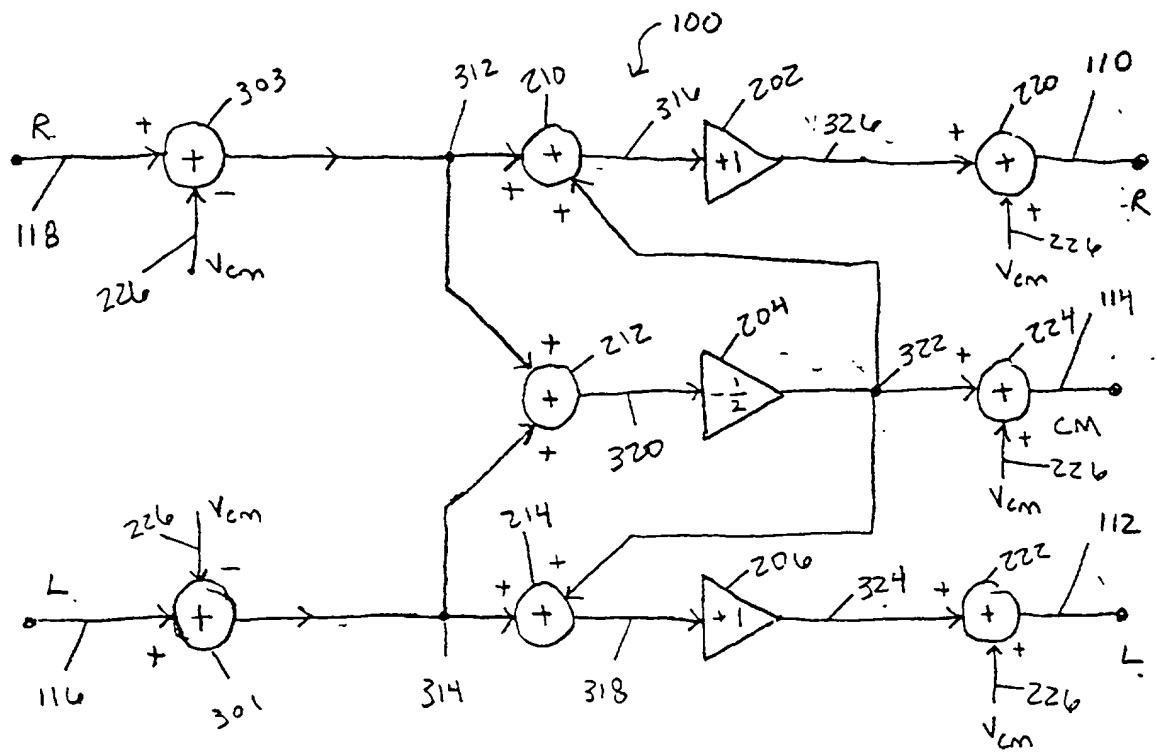


FIG. 3

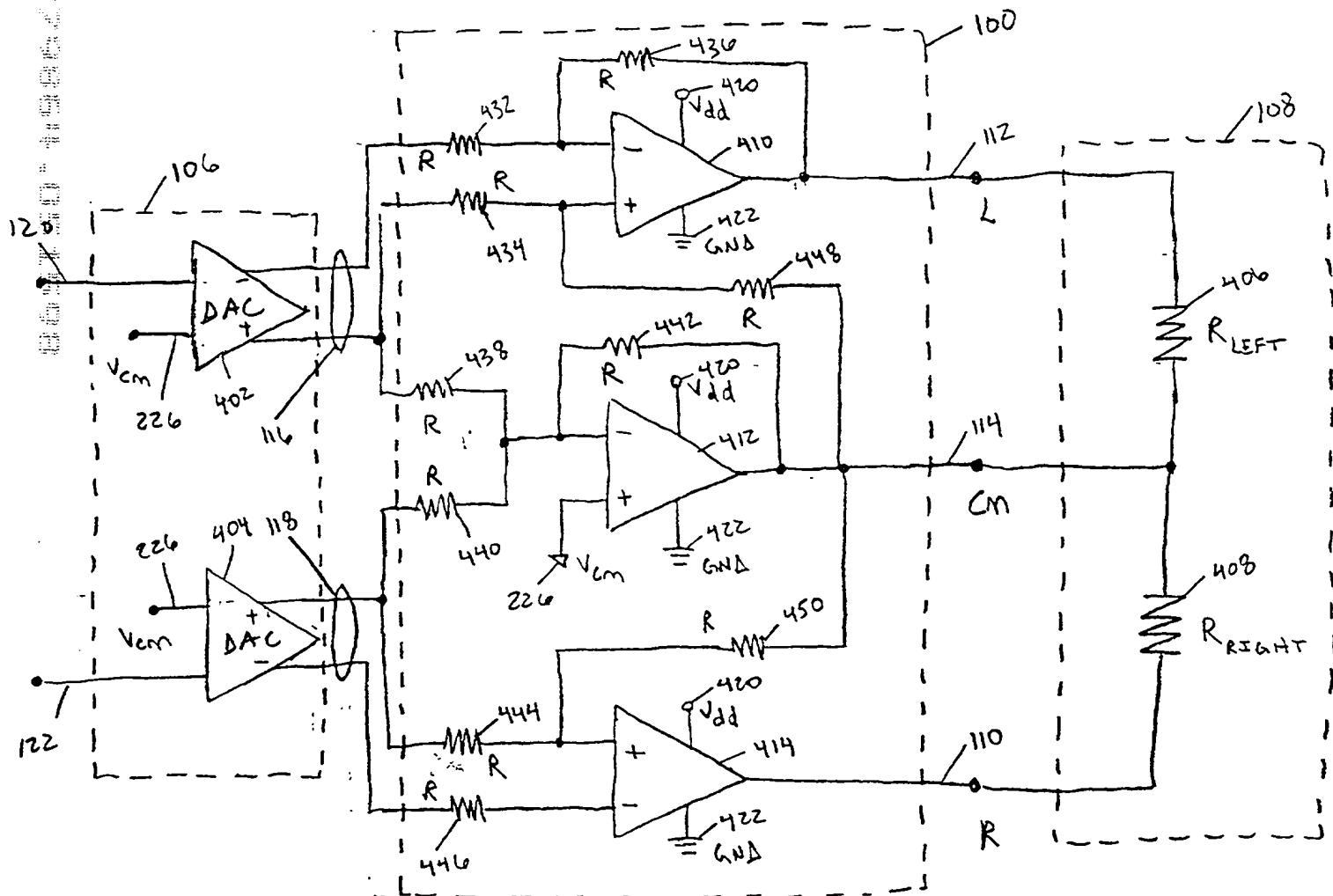


FIG. 4

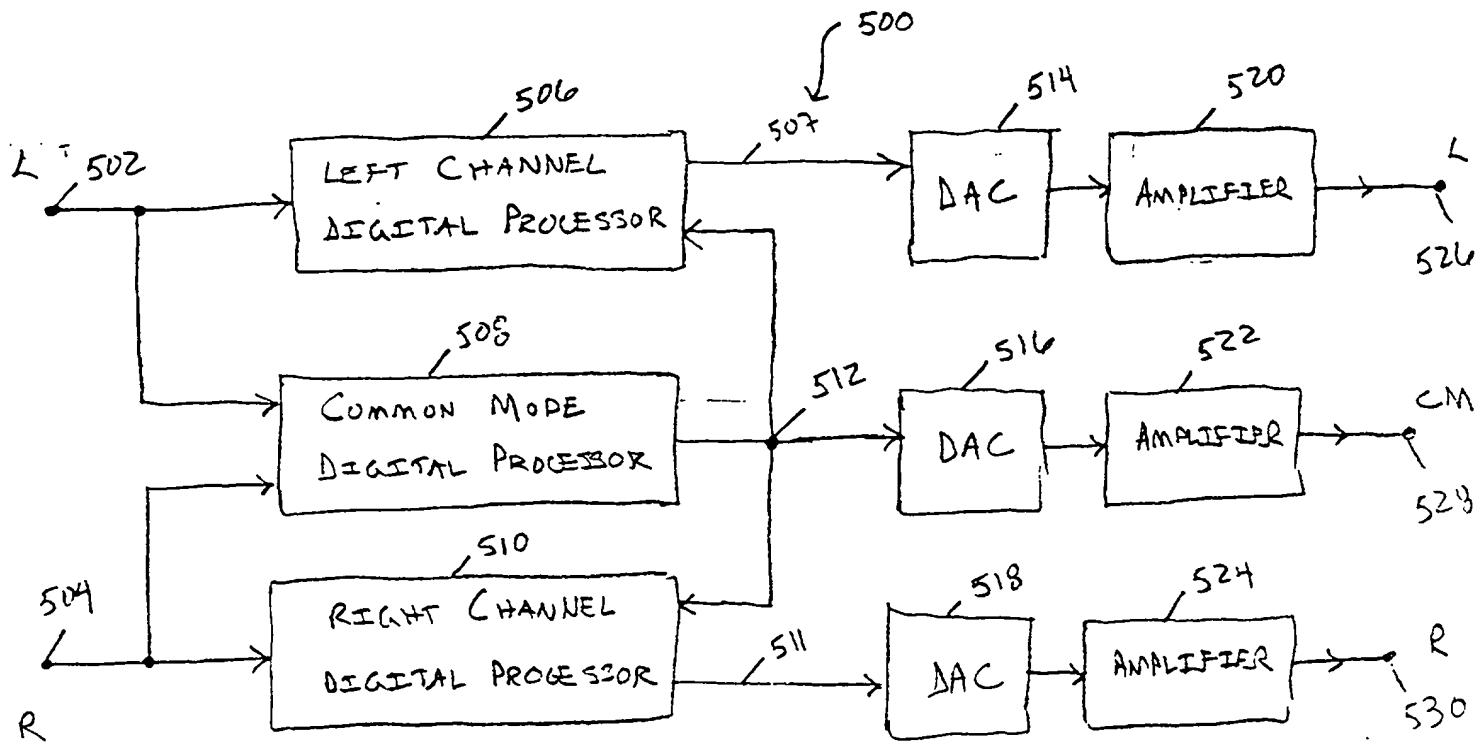


FIG. 5

**DECLARATION FOR PATENT APPLICATION AND
POWER OF ATTORNEY**

As an undersigned inventor, I hereby declare that:

My residence, post office address and country of citizenship are as stated directly below my name.

I believe (check one) I am the original, first and sole inventor
 I am a joint inventor and the below named inventors are the
original and first inventors

of the subject matter which is claimed and for which a patent is sought on the invention entitled

QUASI-DIFFERENTIAL POWER AMPLIFIER AND METHOD

the specification of which

(check one) is attached hereto.
 was filed on _____
as Application Serial No. _____,
and was amended on _____
(if applicable)

I further declare that I have reviewed and understand the contents of the above identified specification, including the claims, as amended by any amendment referred to above.

I acknowledge the duty to disclose to the United States Patent and Trademark Office (the “Office”) all information known to me to be material to patentability of the subject matter which is claimed as defined in 37 C.F.R. §1.56.

I hereby claim foreign priority benefits under 35 U.S.C. § 119 of any foreign application(s) for patent or inventor's certificate indicated below and have also identified below any foreign application for patent or inventor's certificate having a filing date before that of the application on which priority is claimed:

Prior Foreign Application(s)		Day/Month/Year Filed	Claimed	Priority	
Number	Country			Yes	No
_____	_____	_____	_____	_____	X

I hereby claim the benefit under 35 U.S.C. § 120 of any United States application(s) listed below and, insofar as the subject matter of each of the claims of this application is not disclosed in the prior United States application in the manner provided by the first paragraph of 35 U.S.C. § 112,

I acknowledge the duty to disclose to the Office all information known to me to be material to patentability as defined in 37 C.F.R. § 1.56, which became available between the filing date of the prior application and the national or PCT international filing date of this application:

Application Serial No.	Filing Date	Status (patented, pending, abandoned)

The Assignee hereby revokes any previous Powers of Attorney and appoints J. P. Violette, Reg. No. 33,042, Steven A. Shaw, Reg. No. 39,368, Dan Shifrin, Reg. No. 34,473, and Frank D. Nguyen, Reg. No. 39,790, each an attorney with CIRRUS LOGIC, Inc. and Richard D. Egan, Reg. No. 36,788 and Brian W. Peterman, Reg. No. 37,908, each an attorney of the firm of JONES, O'KEEFE & EGAN, as its attorney for so long as they remain with such firm, with full power of substitution and revocation, to prosecute the application, to make alterations and amendments therein, to transact all business in the Patent and Trademark Office in connection therewith, and to receive any Letters Patent, and for one year after issuance of such Letters Patent to file any request for a certificate of correction that may be deemed appropriate.

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I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further, that these statements were made with the knowledge that willful false statements and the like are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code and may jeopardize the validity of the application or any patent issued thereon.

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-- END --